

① Taylor 5.13

Potential energy of a 1-D mass at a distance r is

$$U(r) = U_0 \left(\frac{r}{R} + \lambda^2 \frac{R}{r} \right) \quad \text{for } 0 < r < \infty \text{ with } U_0, R, \lambda \text{ all positive const.}$$

FIND r_0 (equilibrium position)

Let x be the distance from equilibrium, and show that for small x the PE has the form $U = \text{const} + \frac{1}{2} k x^2$

FIND angular frequency for small oscillations

$$U'(r) = U_0 \left(\frac{1}{R} - \lambda^2 \frac{R}{r^2} \right)$$

$$U''(r) = 2U_0 \lambda^2 \frac{R}{r^3}$$

$$U'(r_0) = 0 = U_0 \left(\frac{1}{R} - \lambda^2 \frac{R}{r_0^2} \right)$$

$$0 = \frac{1}{R} - \lambda^2 \frac{R}{r_0^2}$$

$$\lambda^2 \frac{R}{r_0^2} = \frac{1}{R}$$

$$\lambda^2 R^2 = r_0^2$$

$$\boxed{r_0 = \lambda R}$$

$$r = r_0 + x \Rightarrow x = r - r_0$$

use a Taylor series expansion of $U(r) = U(r_0 + x)$

$$U(r_0 + x) = U(r_0) + U'(r_0) x + \frac{1}{2} U''(r_0) x^2 + \dots \text{ H.S.T. negligible higher order terms}$$

$$U(r_0 + x) = U_0 \left(\frac{r_0}{R} + \lambda^2 \frac{R}{r_0} \right) + \frac{1}{2} \left(2U_0 \lambda^2 \frac{R}{r_0^3} \right) x^2$$

$$U(r_0 + x) = U_0 \left(\frac{\lambda R}{R} + \lambda^2 \frac{R}{\lambda R} \right) + \frac{1}{2} \left(2U_0 \lambda^2 \frac{R}{(\lambda R)^3} \right) x^2$$

$$U(r_0 + x) = U_0 (2\lambda) + U_0 \frac{1}{\lambda R^2} x^2$$

$$\boxed{U(r_0 + x) = 2U_0 \lambda + \frac{1}{2} \frac{2U_0}{\lambda R^2} x^2 \Rightarrow U(r) = \text{const} + \frac{1}{2} k x^2 \text{ where } k = \frac{2U_0}{\lambda R^2}}$$

$$\omega = \sqrt{k/m} \Rightarrow$$

$$\boxed{\omega = \sqrt{\frac{2U_0}{m \lambda R^2}}}$$

Taylor 5.30

The position $X(t)$ of an overdamped oscillator is given by

$$X(t) = C_1 e^{-(\beta - \sqrt{\beta^2 - \omega_0^2})t} + C_2 e^{-(\beta + \sqrt{\beta^2 - \omega_0^2})t}$$

a.) Find the constants C_1 and C_2 in terms of X_0 and V_0 :

The velocity equals:

$$\frac{dX(t)}{dt} = V(t) = C_1(-\beta + \sqrt{\beta^2 - \omega_0^2}) e^{-(\beta - \sqrt{\beta^2 - \omega_0^2})t} + C_2(-\beta - \sqrt{\beta^2 - \omega_0^2}) e^{-(\beta + \sqrt{\beta^2 - \omega_0^2})t}$$

$$V(0) = V_0 = C_1(-\beta + \sqrt{\beta^2 - \omega_0^2}) + C_2(-\beta - \sqrt{\beta^2 - \omega_0^2})$$

$$X(0) = X_0 = C_1 + C_2$$

So the system of equations is:

$$X_0 = C_1 + C_2$$

$$V_0 = C_1(-\beta + \sqrt{\beta^2 - \omega_0^2}) + C_2(-\beta - \sqrt{\beta^2 - \omega_0^2}) = -\beta(C_1 + C_2) + \sqrt{\beta^2 - \omega_0^2}(C_1 - C_2)$$

$$V_0 = -\beta X_0 + C_1 \sqrt{\beta^2 - \omega_0^2} - \sqrt{\beta^2 - \omega_0^2} C_2, C_2 = X_0 - C_1$$

$$V_0 = -\beta X_0 + C_1 \sqrt{\beta^2 - \omega_0^2} - \sqrt{\beta^2 - \omega_0^2}(X_0 - C_1)$$

$$V_0 = -\beta X_0 + C_1 \sqrt{\beta^2 - \omega_0^2} + C_1 \sqrt{\beta^2 - \omega_0^2} - X_0 \sqrt{\beta^2 - \omega_0^2}$$

$$-2C_1 = \frac{-\beta X_0 - V_0 - X_0 \sqrt{\beta^2 - \omega_0^2}}{\sqrt{\beta^2 - \omega_0^2}}$$

$$C_1 = \frac{X_0(\beta + \sqrt{\beta^2 - \omega_0^2}) + V_0}{2 \sqrt{\beta^2 - \omega_0^2}}$$

$$C_2 = X_0 - C_1 = X_0 - \frac{X_0(\beta + \sqrt{\beta^2 - \omega_0^2}) + V_0}{2 \sqrt{\beta^2 - \omega_0^2}}$$

$$= \frac{X_0(-\beta + \sqrt{\beta^2 - \omega_0^2}) - V_0}{2 \sqrt{\beta^2 - \omega_0^2}}$$

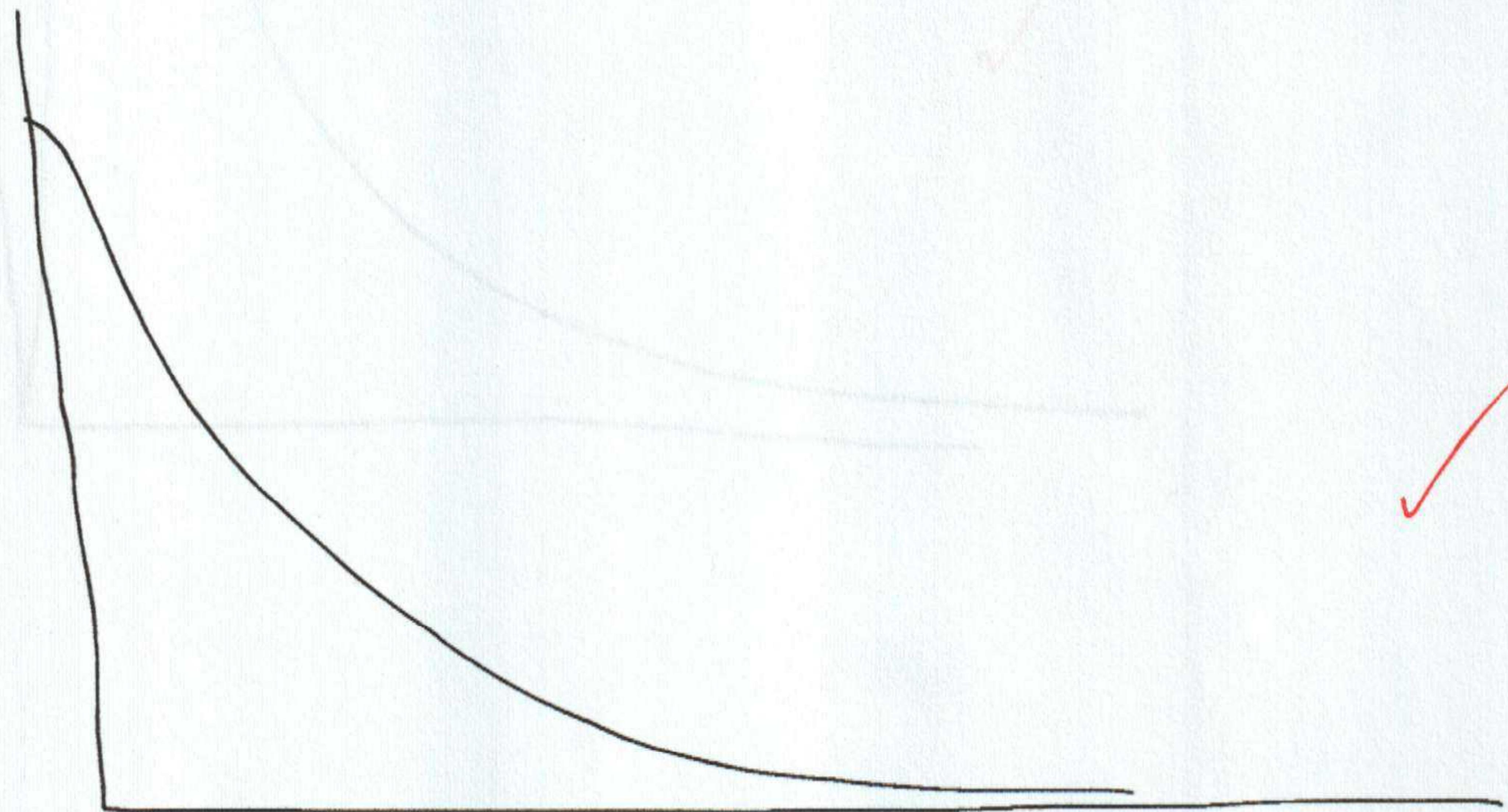
b.) Sketch the behavior of $x(t)$ for the two cases that $V_0=0$ and that $x_0=0$

For $V_0=0$

$$C_1 = \frac{x_0(\beta + \sqrt{\beta^2 - \omega_0^2}) + 0}{2\sqrt{\beta^2 - \omega_0^2}} = \frac{x_0(\beta + \sqrt{\beta^2 - \omega_0^2})}{2\sqrt{\beta^2 - \omega_0^2}}$$

$$C_2 = \frac{x_0(-\beta + \sqrt{\beta^2 - \omega_0^2}) - 0}{2\sqrt{\beta^2 - \omega_0^2}} = \frac{x_0(-\beta + \sqrt{\beta^2 - \omega_0^2})}{2\sqrt{\beta^2 - \omega_0^2}}$$

$$x(t) = C_1 e^{-(\beta - \sqrt{\beta^2 - \omega_0^2}t)} + C_2 e^{-(\beta + \sqrt{\beta^2 - \omega_0^2}t)}$$

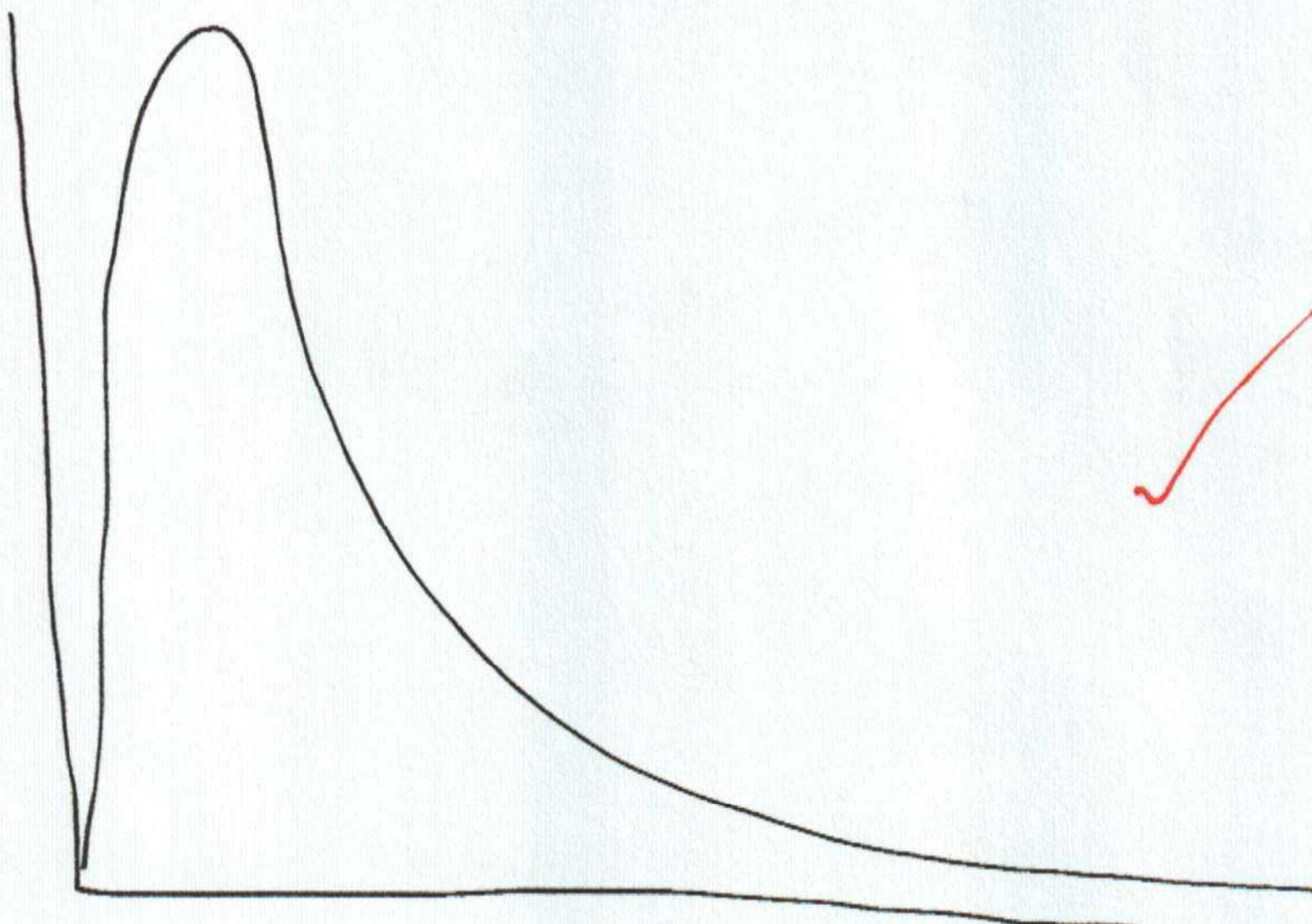


For $X_0 = 0$:

$$C_1 = \frac{0(\beta + \sqrt{\beta^2 - \omega_0^2}) + V_0}{2\sqrt{\beta^2 - \omega_0^2}} = \frac{V_0}{2\sqrt{\beta^2 - \omega_0^2}}$$

$$C_2 = \frac{0(-\beta + \sqrt{\beta^2 - \omega_0^2}) - V_0}{2\sqrt{\beta^2 - \omega_0^2}} = -\frac{V_0}{2\sqrt{\beta^2 - \omega_0^2}}$$

$$x(t) = C_1 e^{-(\beta - \sqrt{\beta^2 - \omega_0^2})t} + C_2 e^{-(\beta + \sqrt{\beta^2 - \omega_0^2})t}$$



c.) Set $\beta \rightarrow 0$, and see $x(t)$ in part (a) approaches the correct solution for undamped motion:

$$x(t) = C_1 e^{-(\beta - \sqrt{\beta^2 - \omega_0^2})t} + C_2 e^{-(\beta + \sqrt{\beta^2 - \omega_0^2})t}$$

$$x(t) = C_1 e^{+\sqrt{-\omega_0^2}t} + C_2 e^{-\sqrt{-\omega_0^2}t}$$

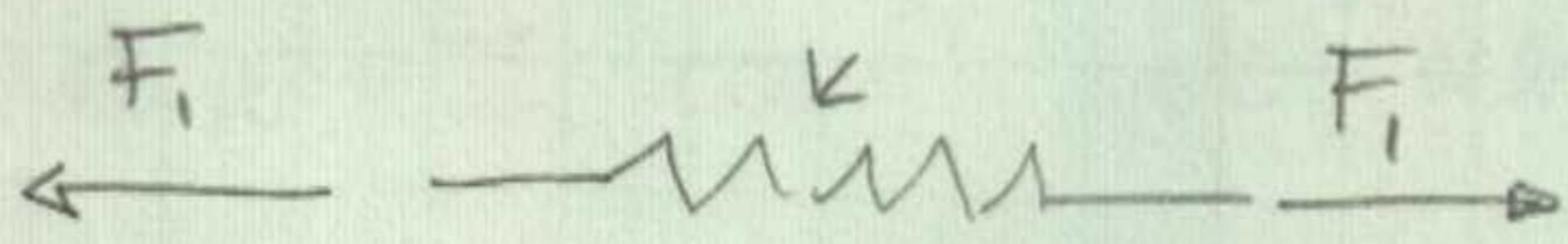
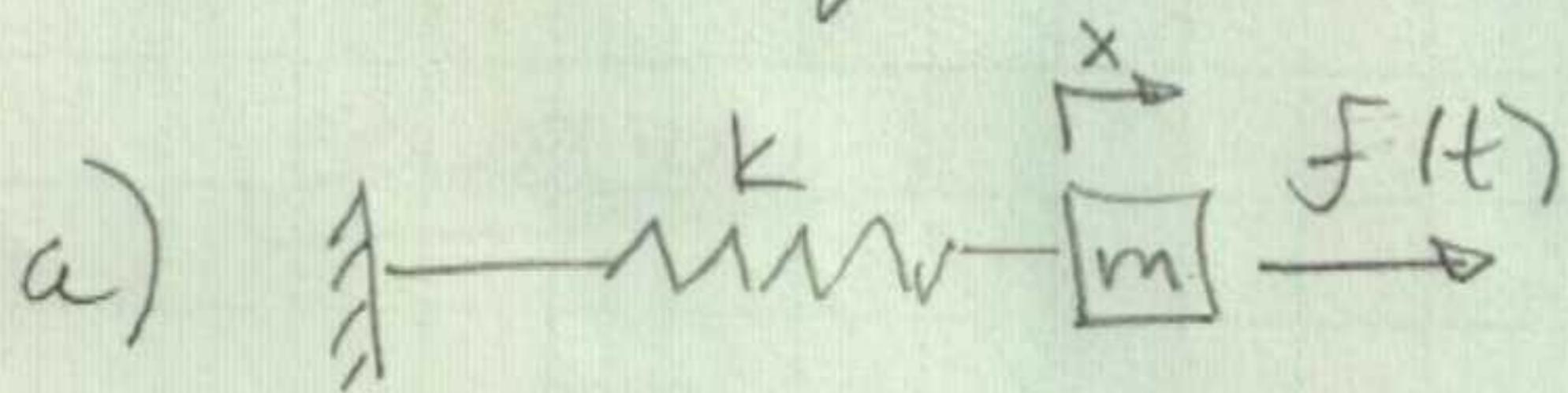
$$x(t) = C_1 e^{+i\omega_0 t} + C_2 e^{-i\omega_0 t}$$

→ undamped ✓

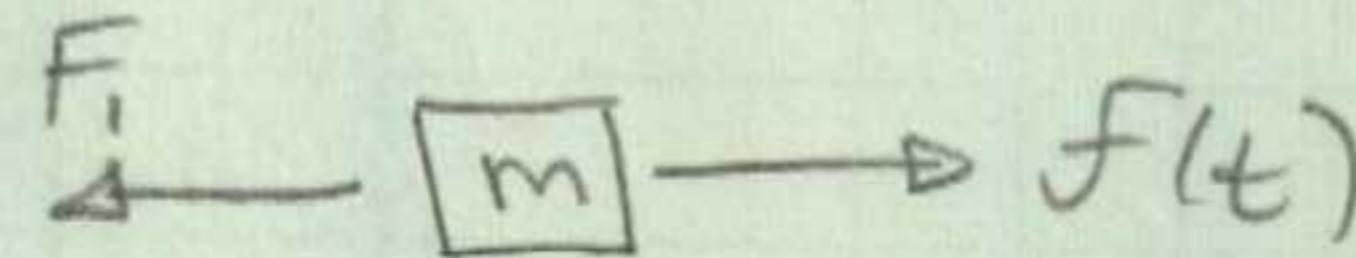
Problem 1.4

(10.1.4)

Find the equation of motion for problems below.

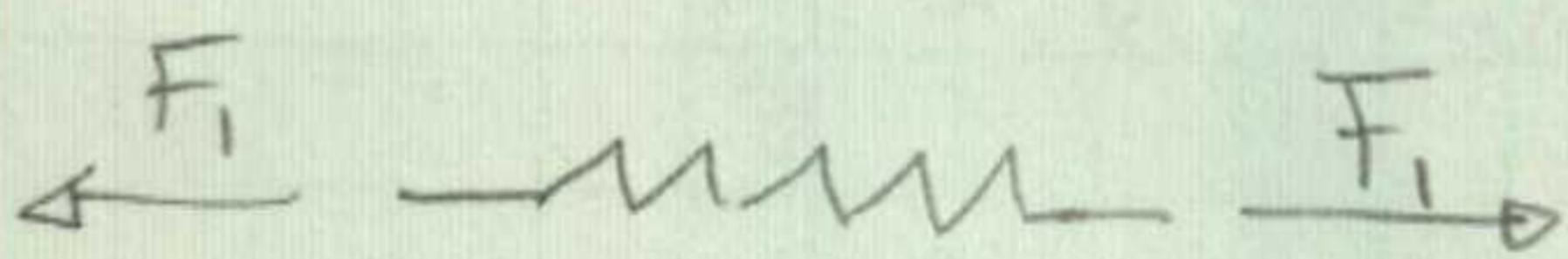
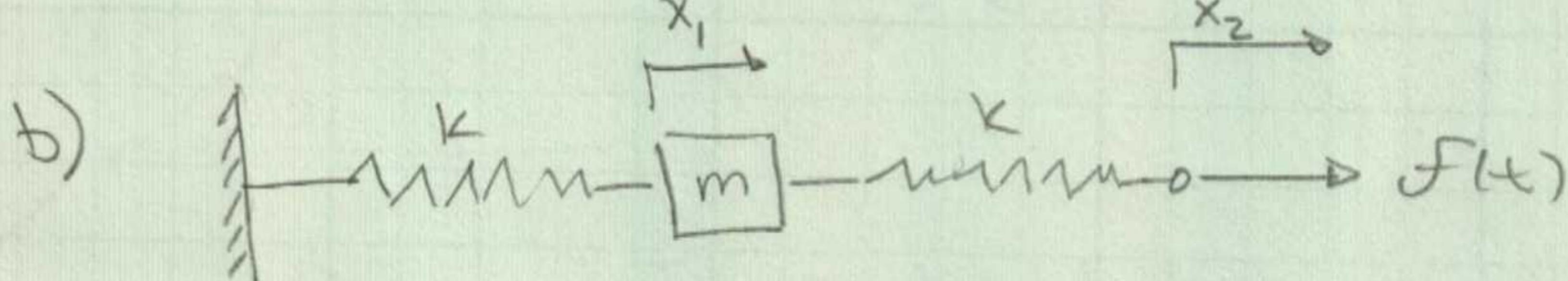


$$F_1 = kx$$

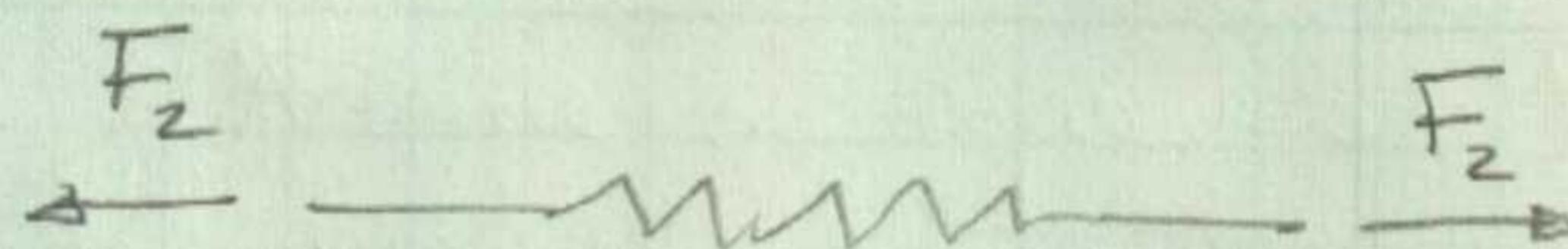


$$\sum \vec{F}_i = m\ddot{x} = f(t) - F_1$$

$$\boxed{m\ddot{x} + kx = f(t)}$$

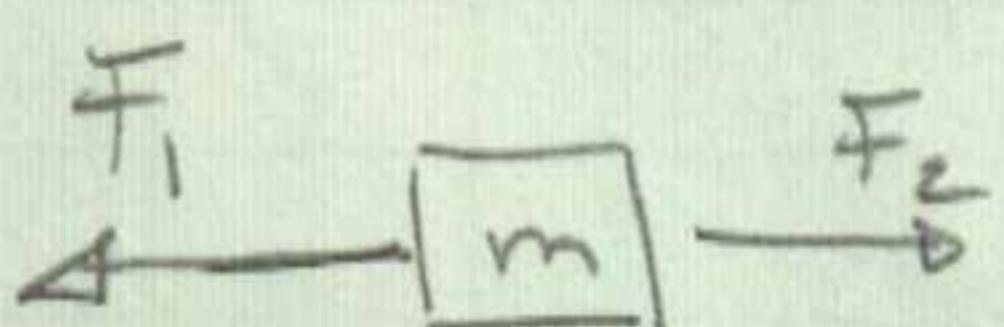


$$F_1 = kx_1$$



$$F_2 = k(x_2 - x_1)$$

Assume a massless bar at the end



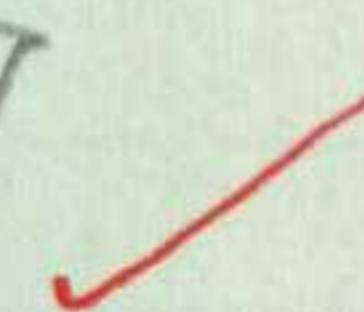
$$\sum \vec{F}_i = m_b \ddot{x}_2 = f(t) - F_2$$

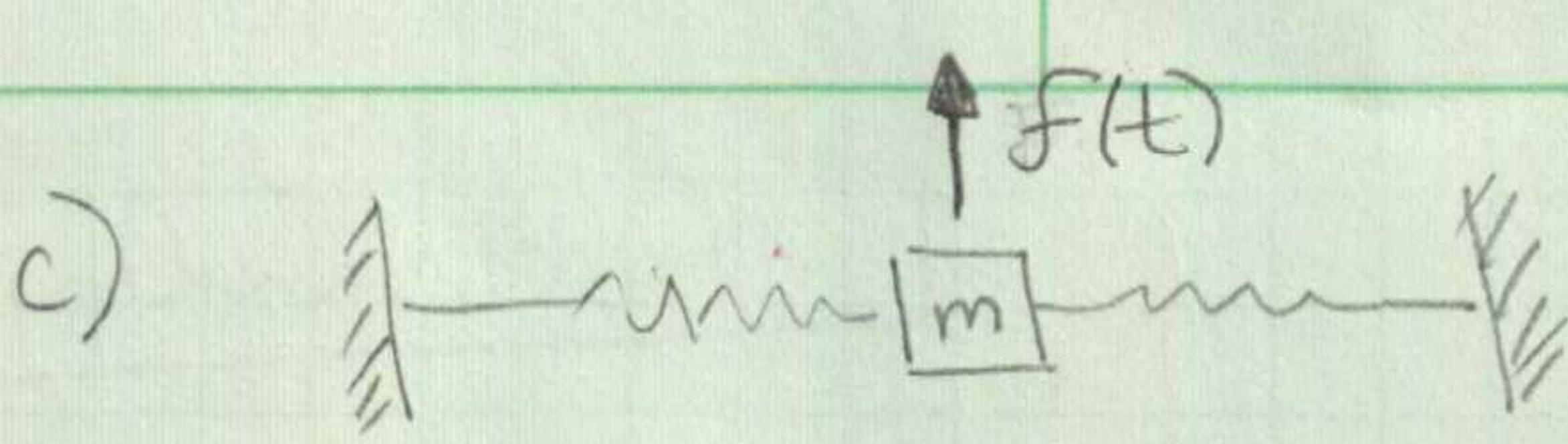
$$F_2 = f(t)$$

$$\sum \vec{F}_i = m\ddot{x}_1 = F_2 - F_1$$

$$m\ddot{x}_1 + F_1 = F_2$$

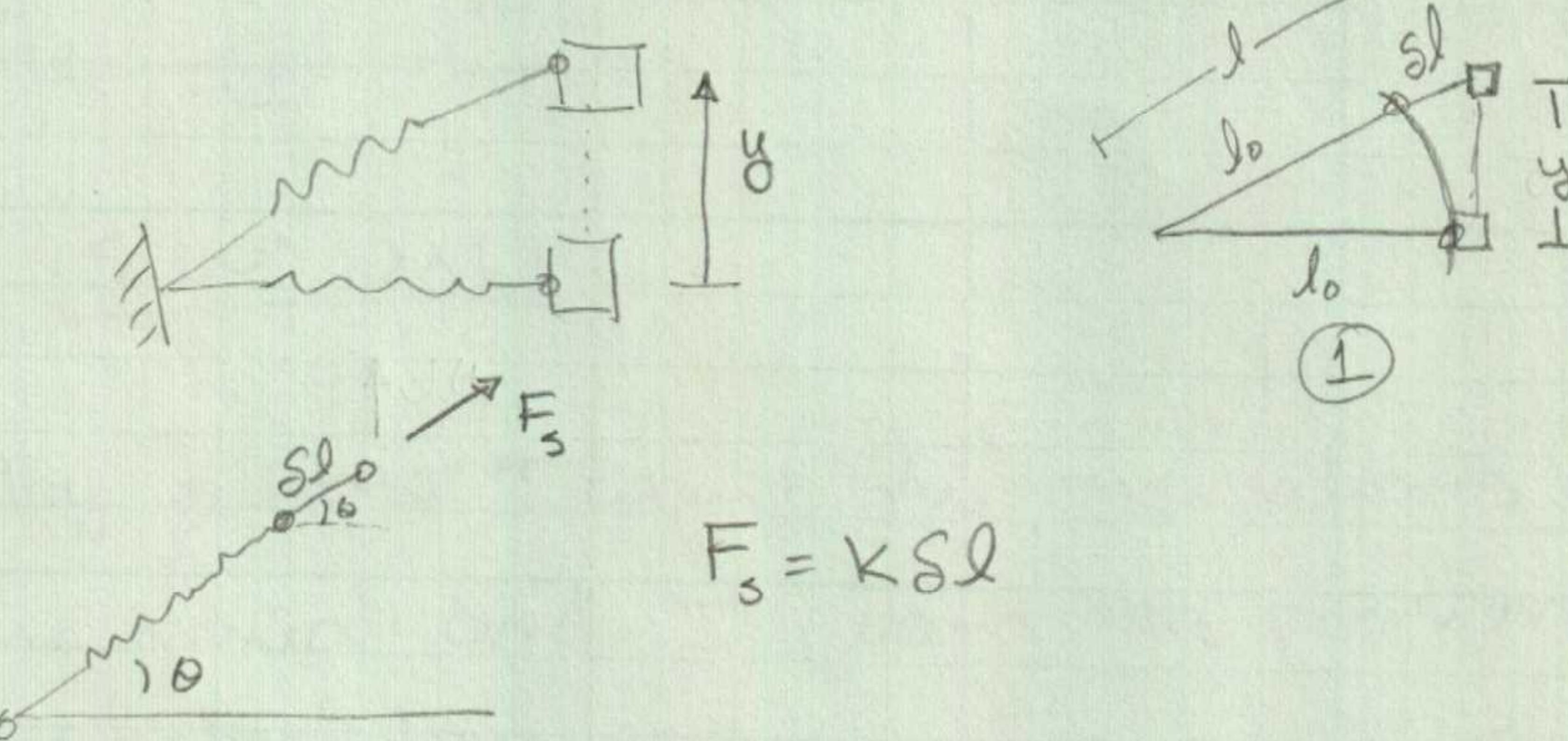
$$\boxed{m\ddot{x} + kx = f(t)}$$





SOLUTION

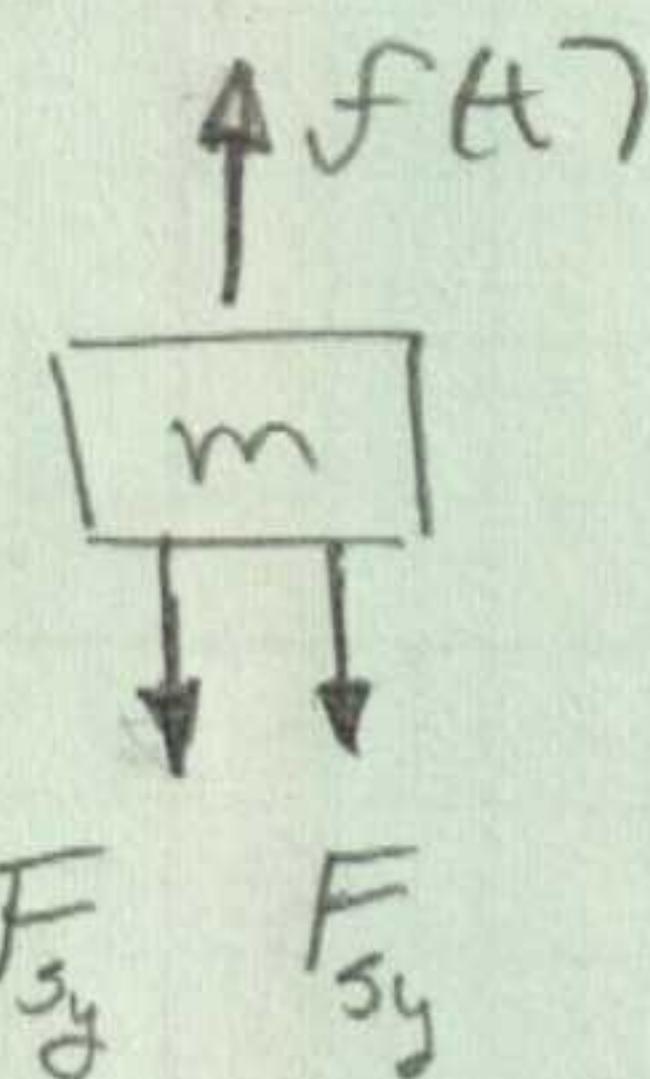
Since the springs are equal length and spring constant equal value I can look at just one.



$$F_s = k \delta l$$

However, I'm interested in the vertical load from the spring.

$$\therefore F_{sy} = k \delta l \sin \theta$$



$$+\uparrow \sum_i F_i = m \ddot{y} = f(t) - 2F_{sy}$$

$$m \ddot{y} + 2k \delta l \sin \theta = f(t)$$

From diagram (1) $\sin \theta = \frac{y}{l_0 + \delta l}$, $l_0^2 + y^2 = l^2 = (l_0 + \delta l)^2$

$$\delta l = \sqrt{l_0^2 + y^2} - l_0$$

$$m \ddot{y} + 2k(\sqrt{l_0^2 + y^2} - l_0) \cdot \frac{y}{\sqrt{l_0^2 + y^2}} = f(t)$$

$$m \ddot{y} + 2k \left(1 - \frac{l_0}{\sqrt{l_0^2 + y^2}}\right) y = f(t)$$

✓

4) RP 10.1.13

$$m = 1 \text{ kg}$$

mass-spring-dashpot system.

$$c = 10 \text{ kg/s}$$

The system returns to its equilibrium position the "quickest" if it hits the approaches the equilibrium the quickest. This will be a critically damped system. To be critically damped, ✓

$$c^2 = 4mk$$

$$100 = 4k$$

$$\therefore k = 25 \text{ kg m/s} \quad \checkmark$$

∴ The stiffness of the spring should be 25 kg m/s.

Tongue

MAB 573°

1.4 Express $2\cos(3t) + 4\sin(3t)$ in terms of e^{3it} and e^{-3it}

Hw 5. 2013/92

Solution: Based on the Trigonometric Identities that:

$$\cos \theta = \frac{1}{2} (e^{i\theta} + e^{-i\theta})$$

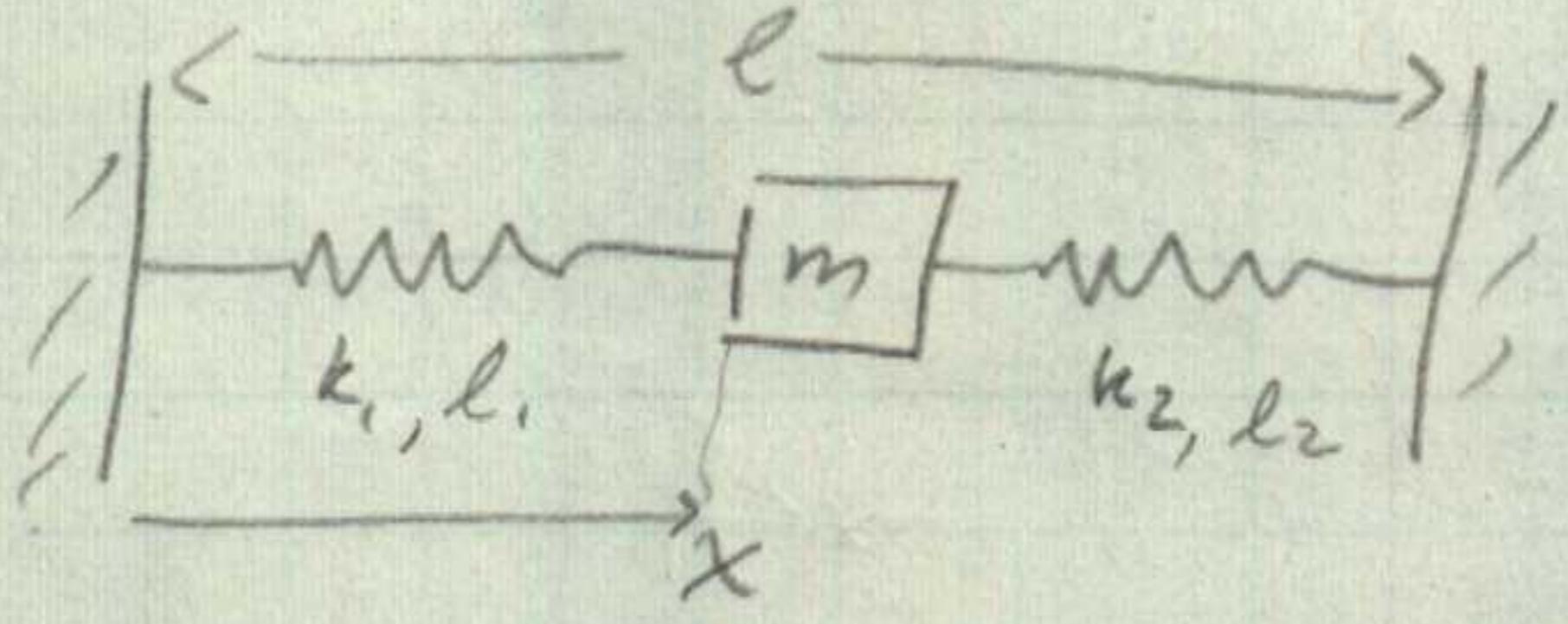
$$\sin \theta = \frac{1}{2i} (e^{i\theta} - e^{-i\theta})$$

Here, we substitute θ with "3t"

then we can get:

$$\begin{aligned}2\cos(3t) + 4\sin(3t) &= 2 \cdot \left[\frac{1}{2} (e^{3it} + e^{-3it}) \right] + 4 \left[\frac{1}{2i} (e^{3it} - e^{-3it}) \right] \\&= \left(1 + \frac{2}{i}\right) e^{3it} + \left(1 - \frac{2}{i}\right) e^{-3it} \\&= (1-2i)e^{3it} + (1+2i)e^{-3it} \quad \checkmark\end{aligned}$$

1.31) The unstretched length of k_1 is 0.5m and the unstretched length of k_2 is 0.25m, $k_1 = 1000 \text{ N/m}$, $k_2 = 2000 \text{ N/m}$, $m = 2 \text{ kg}$, $\ell = 0.5 \text{ m}$. Find the equilibrium position of the mass and determine the natural frequency of the system. Compare this natural freq. to that associated with $\ell = 0.75 \text{ m}$.



$$x + y = l$$

$$y = l - x$$

FBD.

$$\xrightarrow{F_{S_1}} \boxed{\quad} \xrightarrow{F_{S_2}}$$

$$F_{S_1} = -k_1(l_1 - x)$$

$$F_{S_2} = k_2 x (l - x - l_2)$$

LMB: $m\ddot{x} = \sum F$

$$m\ddot{x} = -k_1(l_1 - x) + k_2(l - x - l_2)$$

At x_{eq} , $\ddot{x} = 0$

$$0 = k_1 l_1 - k_1 x_{eq} + k_2 l - k_2 x_{eq} - k_2 l_2$$

$$(k_1 + k_2) x_{eq} = k_1 l_1 + k_2 l - k_2 l_2$$

$$x_{eq} = \frac{(k_1 l_1 + k_2 l - k_2 l_2)}{(k_1 + k_2)} = 0.333 \text{ m}$$

$$m\ddot{x} + (k_1 + k_2)x = k_1 l_1 + k_2(l - l_2)$$

$$\boxed{\omega_0 = \sqrt{\frac{(k_1 + k_2)}{m}} = 38.73 \text{ rad/sec}}$$

ω₀ for $\ell = 0.5 \text{ m}$ or $\ell = 0.75 \text{ m}$ will be the same.